Kinetics and Mechanism of the N₂O Reduction by NH₃ on a Fe-Zeolite-Beta Catalyst

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In the context of decreasing the emissions of greenhouse gases, a Fe-exchanged zeolite-beta (Fe-BEA) catalyst is shown to be very active in the reduction of N₂O by NH₃ in the presence of O₂. The temperature at which 50% N₂O conversion is obtained is lower by ca. 80 K compared to its catalytic decomposition in the absence of NH₃. TPR, TPO, and TPD experiments after treatments in various atmospheres provide evidence that the reaction involves the redox cycle $Fe^{III} \leftrightarrow Fe^{II}$ where the Fe^{III} active species are Fe oxocations of low nuclearity. N₂O decomposes into O* surface species on specific reduced Fe sites with the concurrent release of N₂; these species do not compete with O^* coming from O_2 for their removal by NH_3 . In the absence of O₂, catalytic experiments with ¹⁴N₂O and ¹⁵NH₃ show that: (1) N₂ is mainly formed from ¹⁴N¹⁴N-O splitting to yield ¹⁴N₂, the O^{*} species being in turn removed by ¹⁵NH₃ to give ¹⁵N₂; (2) some ¹⁴N-¹⁴NO bond splitting occurs, which leads to ¹⁴N¹⁵N after reaction of ¹⁴NO* and ¹⁵NH₃ through a classical SCR mechanism. The Fe active species in the N-NO splitting are inhibited in the presence of O₂. The kinetics of N₂O reduction by NH₃ obeys a Mars and van Krevelen oxido-reduction mechanism modified with an inhibiting term of NH₃. © 2000 Academic Press

Key Words: nitrous oxide; ammonia; Fe-zeolite; reduction; mechanism.

INTRODUCTION

Nitrous oxide exhibits a high potential contribution to the greenhouse effect and takes part in the destruction of the stratospheric ozone layer. N₂O is included after CO₂ and CH₄ in the list of "greenhouse gases." At present, every year the N₂O concentration in the atmosphere is rising by 0.25%. The main causes for this increase are anthropogenic activities, such as agriculture and industrial and combustion processes, including emissions from road vehicles. Among industrial processes, the manufacture of adipic acid and nitric acid are the most important emitter of N₂O. At the Kyoto Conference in 1997, the EU committed itself to reduce by 8% in 2010 the emissions of greenhouse gases based on the values of 1990.

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The simplest control technology for N₂O release is based on the catalytic decomposition to N_2 and O_2 (1), and Fezeolite catalysts are among the most active materials in the presence of O₂, though they remain not efficient enough. It was proposed that the decomposition of N₂O over Fezeolites is based on the redox cycle $Fe^{III} \leftrightarrow Fe^{II}$ with the desorption of adsorbed oxygen as the slow step (1). A boosting effect of reductant addition on the decomposition of N_2O was experimentally identified (1–10) and might be interpreted by a faster removal of surface oxygen. It was shown that Fe-ZSM-5 are efficient catalysts for the reduction of N₂O using propane or propene as reductants (4, 6, 10). However, the selectivity of hydrocarbon oxidation to CO was high (4). Moreover, when $NO + N_2O$ mixtures were processed there was a retardation of the onset of N₂O conversion to higher temperatures and the NO conversion levelled off at ca. 40-50% (4). In contrast, when $NO + N_2O$ mixtures were reduced by NH_3 on a Fe-zeolitebeta (Fe-BEA) catalyst, there was a synergistic effect on both the conversion of NO and N₂O which occurred at lower temperature than when processed alone (11); moreover, full NO conversion was reached rapidly. NH₃ is almost always the reductant used in the selective catalytic reduction (SCR) of $NO + NO_2$ mixture from off-gases of power plants and nitric acid plants (12, 13), in which N₂O is often also present. However, no fundamental study exists pertaining to the reduction of N_2O by NH_3 in presence of O_2 . The aim of this work was to elucidate some aspects of the mechanism and the kinetics of this reaction on a Fe-BEA catalyst, in view of developing new active materials at low temperature for N₂O reduction.

EXPERIMENTAL

The Fe-BEA catalyst was prepared by ion exchange of 5 g of H-BEA (Zeolyst PQ Corp., specific surface area \approx 680 m²g⁻¹, Si/Al \approx 12.5, grain size: 120–250 μ m) with 100 cm³ Fe(NO₃)₃ · 9H₂O at a pH of \approx 4. After filtration, the solid was dried at 393 K in an oven and then calcined at 823 K in flowing air overnight (120 cm³ min⁻¹). The chemical analysis was performed at the Service Central d'Analyse



Ar desorption

du CNRS (Vernaison, France) by ICP. The amount of Fe (1.9 wt%) corresponds to a theoretical exchange degree of 97% (300Fe/Al). The nature and the amount of various Fe species were determined by Mössbauer spectroscopy (EG&G) and temperature-programmed reduction experiments by H₂/Ar (TPR). The TPR, TPO (temperatureprogrammed oxidation), and TPD (temperature-programmed desorption) of Fe-BEA activated in various conditions were carried out with a Micromeritics 2910 AutoChem apparatus at 10 K min⁻¹. The detection was performed with TCD and helped by mass spectroscopy coupling when necessary.

Before the catalytic tests, the sample (\approx 200 mg) was reactivated in situ at 823 K in air in a quartz fixed-bed reactor (i.d.: 6 mm, depth of the catalytic bed). The decomposition of N₂O (N₂O/O₂/He = 0.2/3/96.8) and the SCR of N₂O $(N_2O/NH_3/O_2/He = 0.2/0.2/3/96.6)$ were performed in the temperature-programmed surface reaction mode from 300 to 773 K (ramp: 10 K min⁻¹, space velocity: $35,000 h^{-1}$). Experiments with ¹⁵NH₃ and kinetic studies were carried out at the steady state (T = 618 K) in the SCR of N₂O at various space velocities. In the kinetic studies the partial pressures of N₂O, NH₃, and O₂ in the feed were varied in the following ranges: $0 < P(N_2O) < 0.45$ kPa (4500 ppm), $0 < P(NH_3) < 0.4$ kPa (4000 ppm), and $0 < P(O_2) < 4$ kPa (4%). The conversion was then maintained at lower than 20% for using the reactor in the differential mode. The detection was performed with a quadrupole mass spectrometer BALZERS Omnistar and a Bruker Equinox 55 FTIR spectrometer. Nine masses characteristic of NO (30), NO2 $(30, \underline{46}), N_2O (28, 30, \underline{44}), {}^{14}N_2 (\underline{28}), {}^{15}N^{14}N (\underline{29}), {}^{15}N_2 (30),$ NH₃ (17, 18), H₂O (17, 18), O₂ (16, 32), and He (4) were followed. When overlapping occurs in the same masses between several compounds, the contributions of each compound were determined by solving a linear system of equations. Calibrations were done on selected masses and wavelengths before and after each catalytic experiment.

RESULTS AND DISCUSSION

After calcination at 823 K in air, iron in Fe-BEA is distributed as ca. 2% Fe₂O₃ and 98% Fe-containing ions as shown by TPR (Fig. 1) and Mössbauer spectroscopy (doublet with isomer shift at 0.34 and quadrupole splitting at 1.1 mm s⁻¹, characteristic of Fe³⁺ in an octahedral environment). In a TPR experiment the choice of the reducing gas composition (H_2/Ar , 25/75) was done with respect to a balance between reduction of Fe species below 1300 K and sensitivity. In the TPR of Fe-BEA, the peak at 623 K corresponds to the reduction of Fe^{3+} to Fe^{2+} species and of Fe_2O_3 aggregates to Fe₃O₄. The latter species are then reduced to FeO and to Fe⁰ clusters at 870 K. Fe²⁺ reduces to Fe⁰ with collapse of the zeolite network above 1100-1200 K. The H_2 consumption below 800 K is H_2 /Fe 0.42, which provides



FIG. 1. TPR profile of the Fe-BEA. Conditions: H₂/Ar (25/75), $ramp = 10 \text{ K min}^{-1}$.

evidence that a part of the Fe species was still reduced or was unreducible in these conditions. The second proposal is preferred since Mössbauer spectroscopy has not shown any contribution of Fe^{II} species in the starting material. These findings are in good agreement with previous TPR studies on Fe- zeolite materials (14, 15).

The reduction of N_2O by NH_3 in the presence of O_2 on Fe-BEA starts at ca. 570 K and reaches 90% at ca. 650 K (Fig. 2). N₂ and H₂O were only detected as products. The onset of N₂O decomposition occurs at ca. 630 K to yield N_2 and O_2 (Fig. 2). The boosting effect of NH_3 on the N₂O reduction to N₂ is thus evidenced with a decrease of the light-off temperature (50% of N₂O conversion) by



FIG. 2. SCR of N₂O by NH₃ (O) and N₂O decomposition (\diamond) as a function of temperature on Fe-BEA. Conditions: SCR of N_2O , $N_2O/NH_3/O_2/He = 0.2/0.2/3/99.6$; N_2O decomposition, $N_2O/O_2/He = 0.2/0.2/3/99.6$; $N_2O/O_2/2/99.6$; $N_2O/O_2/99.6$; $N_2O/O_2/99.6$; N_2O 0.2/3/99.8; ramp = 10 K min⁻¹, space velocity = 35,000 h⁻¹.

1400

1200

1000

ca. 80 K compared to that of N_2O decomposition. We have previously reported that the promoting effect of NH_3 on N_2O reduction on Fe-zeolite depended on the nature of the zeolite (16). It was very low for Fe-FER, but the largest for Fe-BEA and Fe-MFI.

In its simplest form the catalytic decomposition of N_2O has been described by Eqs. [1]–[3] (1, 17):

$$N_2O + ^* \rightarrow N_2 + O^*$$
 [1]

$$N_2O + O^* \rightarrow N_2 + O_2 + ^*$$
 [2]

$$2O^* \leftrightarrow O_2 + 2^*$$
. [3]

In the presence of NH₃, the surface oxygen can also be removed according to Eq. [4]:

$$2NH_3 + 3O^* \rightarrow N_2 + 3H_2O + 3^*$$
. [4]

It should be pointed out that a possible small release of O_2 , according to Eqs. [1] and [2], might not be identified in the SCR of N_2O by NH_3 due to the large excess of O_2 . However, N_2O reduction by NH_3 in the absence of O_2 has not shown any formation of O_2 below 740 K, and the stoichiometry of the reaction was $N_2O/NH_3 \approx 3/2$. This is a strong argument that allows one to postulate that since no O_2 release occurred during the reduction of N_2O by NH_3 in the absence of O_2 , this very likely remains true when O_2 is present in the feed. There is thus no interference between the SCR of N_2O by NH_3 and its catalytic decomposition below 620 K.

The influence of O_2 content on N_2O and NH_3 conversion rates was first studied by classical kinetics at 618 K and steady state; no deactivation was observed. The rate of N_2O reduction only increased very slightly with O_2 content



FIG. 3. Rates of N₂O reduction by NH₃ (\Box) and of NH₃ oxidation (\bigcirc) as a function of *P*(O₂) on Fe-BEA. Conditions: *T*_R = 618 K, space velocity = 25,000–35,000 h⁻¹, *P*(N₂O) = *P*(NH₃) = 0.2 kPa, balance with He.



FIG. 4. (a) TPD from Fe-BEA calcined in O_2/N_2 (20/80) at 773 K. (b) TPD from Fe-BEA activated in N_2O/He (5/95) at 773 K after reduction in H_2/Ar (25/75) at 773 K. Conditions: ramp = 10 K min⁻¹.

(Fig. 3). The inhibition by O_2 of the N_2O reduction, when occurring, could be understood by Eq. [3] backward. This inhibition is generally low for Fe species exchanged in a zeolite matrix (1, 7), and this is confirmed for the present Fe-BEA catalyst. In contrast, O₂ accelerated sharply the oxidation of NH₃ to N₂, which reached a plateau above 2000 ppm O_2 (Fig. 3). This behavior likely means that NH_3 reacts with two different surface oxygens in Eq. [4], coming either from N_2O or from O_2 . This can be correlated with the different TPD profiles from Fe-BEA calcined in O_2/N_2 (20/80) at 773 K (Fig. 4a) on the one hand and activated at 773 K in N₂O/He (5/95) after reduction at 773 K in H_2/Ar (25/75) on the other hand (Fig. 4b). One should be precise in that after activation at 773 K in N₂O/He the sample was cooled to room temperature in the same gas. After calcination in O₂/N₂, a broad peak of O₂ desorption with shoulders appears in the range 800-1100 K. After activation in N₂O/He of the reduced Fe-BEA, there is always a broad peak of O_2 desorption at high temperature (>800 K) but several other desorption peaks of large magnitude appeared at lower temperatures. The natures of desorbing species were identified by mass spectroscopy, which allowed one to attribute desorption peaks to N₂O at 450 K and to NO at ca. 660 K and three peaks of O₂ desorption at 610, 790, and 940 K. It clearly appears that a different surface oxygen exists after N₂O treatment, which desorbs in a significant amount at low temperature (\approx 610 K). One may speculate that this surface oxygen is analogous to that proposed to be formed by interaction of N₂O with Fe-ZSM-5 zeolite and called α -oxygen (18). These species were proposed to be associated with binuclear Fe complexes rather than with isolated atoms (19).

In the reduction of N₂O by NH₃ we normally expected that the reaction was regulated by Eqs. [1] and [4] since O₂ formation was never detected. In a reaction of ¹⁴N₂O with ¹⁵NH₃, the isotopic distribution of labelled dinitrogen isotopomers would therefore be 25% ¹⁵N₂ and 75% ¹⁴N₂. Since O_2 has little influence on the rate of N_2O reaction with NH₃, we first carried out the reduction of $^{14}N_2O$ by ¹⁵NH₃ in the absence of O₂ (618 K, steady state conditions, high N₂O conversion by tuning the space velocity). The distribution of N₂ isotopomers is shown in Fig. 5 as a function of time. Surprisingly, about 17% ¹⁴N¹⁵N was thus formed, which could not be taken into account by Eqs. [1] and [4]. However, when the same experiment was carried out in an O₂-rich atmosphere, the amount of ¹⁴N¹⁵N did not exceed 2% (Fig. 5). When the isotopomer was switched from $^{15}NH_3$ to $^{14}NH_3$, the proportion of $^{14}N^{15}N$ went through a

1.0

FIG. 5. Distribution of N₂ isotopomers in the reduction of ¹⁴N₂O, from 0 to 1000 s by ¹⁵NH₃ and then by ¹⁴NH₃, on Fe-BEA: (a) without O₂, (b) with 3% O₂. Conditions: $T_{\rm R} = 618$ K, $P(\rm N_2O) = P(\rm NH_3) = 0.2$ kPa, space velocity \approx 10,000 h⁻¹.

maximum before decreasing to zero. This is a transient phenomenon due to substitution of adsorbed ¹⁵NH₃ by ¹⁴NH₃; ¹⁵NH₃ and ¹⁴NH₃, both present on the surface, then react according to Eq. [4] to yield ¹⁴N¹⁵N.

N-NO splitting would normally lead to NO and N₂. NO was not identified in the course of the reaction, but in the TPD from Fe-BEA after N₂O treatment (Fig. 4b), an NO desorption peak indeed appeared at 660 K. Moreover, we have shown that the SCR of NO in the presence of N₂O $(NO/N_2O < 1)$ is extremely fast on Fe-BEA, even in the absence of O_2 (11). This could explain why NO has not been detected in the effluent during the catalytic experiments. These results suggest that a minor reaction, which may be described stoichiometrically as $2N_2O \rightarrow N_2 + 2NO$, may also occur by breaking of the much stronger N-NO bond (481 kJ mol⁻¹) rather than the weaker NN-O bond (167 kJ mol⁻¹). Such a reaction was evidenced recently in the decomposition of N₂O on Ba/MgO (20). The desorption of NO at ca. 610 K has also been identified in the TPD of Fe-ZSM-5 after exposure to N₂O at 473 K (21).

We can thus propose that the reduction of N_2O by NH_3 very likely proceeds according to a redox cycle of "Fe ions" involving N_2O and NH_3 as an oxidant and reductant interacting on separated sites with the splitting on the NN-O bond in N_2O . A minor contribution exists, coming from N-NO splitting and the subsequent SCR of NO by NH_3 . The iron sites responsible for the N-NO bond splitting are inhibited in the presence of O_2 .

Temperature-programmed reduction and oxidation experiments were carried out to obtain more insight into the redox mechanism. In these experiments, the nature of released gases was followed by mass spectroscopy detection. We wished first to carry out TPO by N₂O after activation of Fe-BEA in NH₃. Actually, NH₃ remained too strongly bonded on the catalyst and desorbed up to 1100 K (22). This behavior alters the results since the reaction $NH_3 + N_2O$ then superimposes to the oxidation of reduced Fe species by N₂O. However, additional experiments have shown that after reduction by NH₃/He (0.2/99.8) at 773 K of Fe-BEA, there was no more H₂ consumption when TPR was carried out up to 773 K in H_2/Ar (25/75). We have then concluded that the reduction state of the Fe species is very similar when Fe-BEA is activated at 773 K in NH₃/He (0.2/99.8) or H₂/Ar (25/75). TPO by N₂O/He (0.2/99.8) was therefore carried out after activation of Fe-BEA in H₂/Ar (25/75) at 773 K. The TPO profile (Fig. 6a) shows two waves of N₂O consumption:

(1) The first N₂O consumption occurs at medium temperatures (473–673 K), with the release of N₂ only, and corresponds to the specific interaction between N₂O and reduced Fe sites with the anchoring of O^{*}. As compared to the total Fe content, N₂O consumption is N₂O/Fe \approx 0.52 (mol/mol). It is however important to keep in mind that



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FIG. 6. (a) TPO by N₂O/He (0.2/99.8) of Fe-BEA after reduction in H₂/Ar (25/75) at 773 K. (b) TPR by NH₃/He (0.2/99.8) of Fe-BEA after oxidation in N₂O/He (0.2/99.8) at 773 K. Conditions: ramp = 10 K min⁻¹, space velocity = 10,000 h⁻¹, mass spectroscopy detection.

a part of the Fe³⁺ species was not reduced by treatment in H_2/Ar (25/75), as the TPR experiment showed (Fig. 1, *vide supra*); on that account, the actual consumption of N_2O per reduced "Fe site" is likely in the range 0.5–1.

(2) The onset of the second N_2O consumption starts around 650 K and corresponds to the initiation of the catalytic decomposition of N_2O into N_2 and O_2 .

TPR by NH₃/He (0.2/99.8) has been carried out after oxidation by N₂O/He (0.2/99.8) at 773 K of Fe-BEA previously reduced (Fig. 6b). In the course of TPR, very strong adsorption of NH₃ made its concentration profile uninformative. In contrast, the release of N₂ formed is very clear and occurs as a broad peak with shoulders between 373 and 773 K. The expected H₂O released is delayed due to retention on the BEA zeolite. As compared to the total Fe content, the N₂ formation is N₂/Fe \approx 0.20 (mol/mol), which corresponds to an NH₃ consumption of NH₃/Fe \approx 0.40.

If one compares the two profiles of TPR by NH_3 and TPO by N_2O (Fig. 6), it is worth to noting that the onset

of the TPR profile occurs at lower temperatures. One might speculate that in the oxido–reduction cycle of iron, which regulates the reaction $N_2O + NH_3$, the oxidation of the reduced Fe sites by N_2O would likely be the rate-determining step. Moreover, we can also notice that in the course of the TPO/TPR sequence the normalised N_2O/Fe and NH_3/Fe consumptions are in very good agreement with the stoichiometry $N_2O/NH_3=3/2$ of the global reaction $3N_2O+2NH_3 \rightarrow 4N_2+3H_2O.$

In the very classical kinetic treatment of oxido–reduction reactions by Mars and van Krevelen (23), the rate law of the reaction $N_2O + NH_3$ will take the following form: $r = k_1 P(N_2O)k_2 P(NH_3)/[k_1 P(N_2O + k_2 P(NH_3)]]$. The rate dependency as a function of N_2O content (Fig. 7) in the feed is in agreement with this kinetic law. In contrast, the evolution of the rate as a function of NH_3 content (Fig. 8) does not obey this kinetic law and goes through a maximum value for $P(NH_3) \approx 0.06$ kPa (600 ppm). Taking into account that NH_3 is strongly bonded on Fe-BEA (20), an inhibiting effect of NH_3 on the oxidation of reduced Fe sites can be considered. Since the precise nature of reduced and oxidized Fe sites could not be identified, in the following we will denote these sites as "Fe^{II}" and "Fe^{III}–O", respectively. The following reaction sequence can be proposed:

-reduction of
$$N_2O$$
: N_2O + "Fe^{II}"

$$\stackrel{{}^{k_1}}{\longrightarrow} N_2 + "Fe^{III} - O"$$
 [5]

—oxidation of NH_3 : $2/3NH_3 + "Fe^{III} - O"$

$$\xrightarrow{k_2} 1/3N_2 + "Fe^{II}" + H_2O \quad [6]$$

[7]

-adsorption of NH₃: "Fe^{II}" + α NH₃ $\stackrel{\lambda_1}{\longleftrightarrow}$ "Fe^{II}" (NH₂) $_{\alpha}$.



FIG. 7. Rate of N₂O reduction by NH₃ on Fe-BEA as a function of P(N₂O). Conditions: $T_{\rm R} = 618$ K, space velocity = 25,000–35,000 h⁻¹, $P(\rm NH_3) = 0.2$ kPa, $P(\rm O_2) = 3$ kPa, balance with He.



FIG. 8. Rate of N₂O reduction by NH₃ on Fe-BEA as a function of $P(NH_3)$. Conditions: $T_R = 618$ K, space velocity = 10,000–50,000 h⁻¹, $P(N_2O) = 0.2$ kPa, $P(O_2) = 3$ kPa, balance with He.

This is a very simplified approach that is only aimed at demonstrating that an inhibiting term in NH_3 can account for a volcano-shaped dependency of the rate versus NH_3 pressure. Assuming that the "Fe^{II}" (NH_3)_{α} species exhibit very low reactivity to be reoxidized by N_2O directly, compared to "Fe^{II}", the following rate expression can be derived from a classical kinetic treatment:

$$r = \frac{k_1 P_{N_2O} k_2 P_{NH_3}^{2/3}}{k_1 P_{N_2O} + k_2 \left[1 + \lambda_1 P_{NH_3}^{\alpha}\right] P_{NH_3}^{2/3}}.$$
 [8]

One can see that the partial order with respect to N_2O varies from 1 to 0 when the N_2O pressure increases, in agreement with data from Fig. 7. Moreover, Eq. [8] indeed accounts for the volcano-shaped dependency of the rate with the NH_3 pressure. However, the determination of rate and adsorption constants as well as the α exponant would need a much more detailed and dedicated kinetic study, which has not yet been undertaken.

CONCLUSION

The present study has demonstrated that NH₃ accelerates the reduction of N₂O to N₂ on Fe-BEA. In the presence of O₂ we propose that N₂O conversion occurs through the redox cycle Fe^{III} \leftrightarrow Fe^{II} with NN–O splitting mainly. N₂O oxidizes Fe^{II} to lead Fe^{III}-oxocations, which are regenerated back to Fe^{II} by NH₃. However, significant N–NO splitting occurs in the absence of O₂. There is no inhibiting effect of O₂ for the reduction of N₂O by NH₃, which obeys a modified Mars and van Krevelen oxido–reduction kinetics, taking into account an inhibiting term of NH₃.

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